

Modelling and Optimisation of a Relativistic Magnetron with Transparent Cathode with TE_{11} -mode Emission of Microwaves

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This paper presents particle-in-cell (PIC) simulations of a relativistic magnetron (RM) using a transparent cathode configuration. The RM is a device capable of generating pulsed high-power microwaves (HPM). Previous research on RMs with transparent cathode has shown favourable results regarding efficiency and oscillation rise time. In [1], Fuks et al. showed with PIC simulations an RM with a transparent cathode capable of generating HPM in the gigawatt-range with high efficiency, short rise time of oscillations, and a TE_{31} -mode. This design was experimentally tested by Leach et al. [2].

In this work, a modified diffraction output is used combined with a smaller waveguide radius in order to obtain microwaves with a clean TE_{11} -mode. We show that this design can achieve a relatively high efficiency of $\sim 37\%$ at 2.57 GHz with a peak output power of 1.1 GW , having a rise time of $\sim 13\text{ ns}$. The diffraction output consists of two pairs of large cavities and one pair of small cavities, as shown in Figure 1(b). Such a geometry will convert the favourable π mode (i.e. the cavity mode that is excited in the interaction region) to a TE_{11} -mode at the cylindrical waveguide [3]. Additionally, the waveguide radius is kept relatively small at $r = 7\text{ cm}$ to reduce the possibility of exciting higher-order modes such as TM_{11} and TE_{01} . This is advantageous for the RM operating around a desired frequency of $2.50 - 2.58\text{ GHz}$. Parameter studies were done using PIC simulations in MAGIC3D to determine the optimal geometrical specifications for the RM. The parameters studied were the transparent cathode orientation θ ($\theta = 0^\circ$ implies that the cathodes are in direct alignment with the centres of the anode cavities), length of interaction region L_{int} , and length of emitter $L_{emitter}$. The studies concluded that optimal values are $\theta = 15^\circ$, $L_{int} = 13.5\text{ cm}$, $L_{emitter} = 4.5\text{ cm}$.

In order to understand the electron dynamics and to find the optimal beam-to-microwave efficiency η and peak output power P_{max} , we chose to study two separate magnetic field strengths ($B = 0.28\text{ T}$ and $B = 0.34\text{ T}$) for various applied voltages V_{ac} over the anode-cathode (A-K) gap. The magnetic field strength B is generated by a set of Helmholtz coils placed symmetrically around the emitter, having the radius $R_{coil} = 8\text{ cm}$ in order to be placed outside the RM easily. The input power P_{in} is defined as $P_{in} = V_{ac} \cdot I_c$, where I_c is the net current in the cathode while P_{max} is defined as the maximum value of the output power P_{out} (when V_{ac} has reached steady state). Since P_{out} oscillates, the beam-to-microwave efficiency is defined as $\eta = \overline{P_{out}}/P_{in}$ (where the bar symbol denotes time average). The applied voltage V_{ac} was modelled as a ramp function with a rise time of $t_{rise} = 4\text{ ns}$. In Figure 2(a), we show that there is an optimal range for the voltage V_{ac} for a given value of B where a TE_{11} mode is excited. If V_{ac} is too low, there is either no microwave excitation or excitation of a different mode but at low efficiency. This is shown in Figure 2(a), where a TE_{21} mode was excited for $B = 0.28\text{ T}$ at $V_{ac} = 205\text{ kV}$ and $B = 0.34\text{ T}$ at $V_{ac} = 258\text{ kV}$. For higher values of V_{ac} , we cross the Bunemann-Hartree condition for a different cavity mode in the interaction region, here denoted f_2 , which becomes dominant and results in the excitation of a TE_{21} mode. This is illustrated in Figure 2(a) for $B = 0.34\text{ T}$ and $V_{ac} > 332\text{ kV}$.

The highest efficiency of $\eta = 37.0\%$ occurs at $V_{ac} = 318\text{ kV}$ and $B = 0.34\text{ T}$, having a peak output power of $P_{max} = 960\text{ MW}$. However, the highest $P_{max} = 1.1\text{ GW}$ occurs at $V_{ac} = 328\text{ kV}$ and $B = 0.34\text{ T}$, with a slightly lower $\eta = 36.5\%$. For the lower value of $B = 0.28\text{ T}$, the highest efficiency of $\eta = 35.4\%$ is found when $V_{ac} = 234\text{ kV}$, resulting in $P_{max} = 410\text{ MW}$. The input power, output power, and average output power for the highest performing case are shown in Fig.2(b). After $\sim 11\text{ ns}$, the input power stabilises at $P_{in} = 1.55\text{ GW}$ while the output power stabilises after $\sim 13\text{ ns}$. The frequency of the resulting TE_{11} mode is 2.57 GHz , which is well above the cutoff frequency of the π mode in the interaction region at 2.53 GHz . For the cases where the TE_{21} mode was excited for lower V_{ac} , the frequency increased to 2.73 GHz for $B = 0.28\text{ T}$ and 2.61 GHz for $B = 0.34\text{ T}$. On the other hand, excitation of the TE_{21} mode for higher V_{ac} resulted in a lower frequency of 2.37 GHz for both values of B . In Figure 3, the voltage V_{ac} and impedance Z_{ac} are shown for the two best simulations for each value of B . The voltages for both cases rise to a maximum after $\sim 6\text{ ns}$ but decrease due to a current flow between the A-K gap and hence an impedance drop. The impedance for the case of $B = 0.34\text{ T}$ settles at $Z_{ac} = 69\text{ }\Omega$ after $\sim 12\text{ ns}$, while the impedance for $B = 0.28\text{ T}$ is significantly higher at $Z_{ac} = 91\text{ }\Omega$ and settles after a longer time of $\sim 16\text{ ns}$.

In conclusion, we have shown that the transparent cathode configuration for an RM is a design worth investigating further. The short rise time of $\sim 13\text{ ns}$ is favourable for RMs, as well as the relatively high efficiency of $\eta = 37\%$ and peak output power of $P_{max} = 1.1\text{ GW}$.

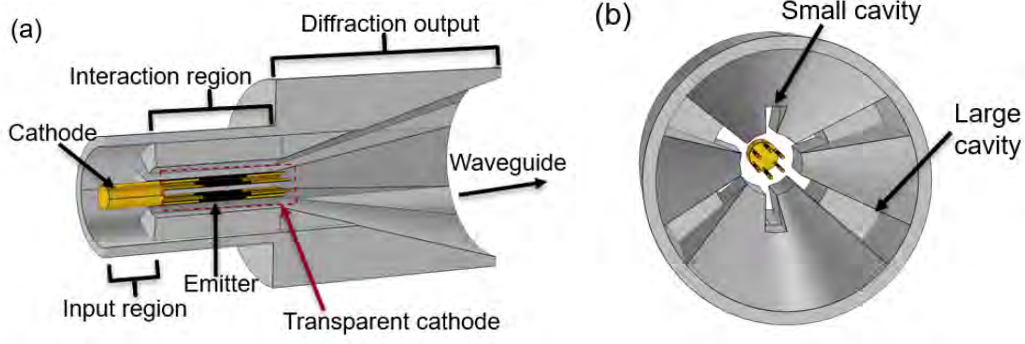


Figure 1. a) 3D cross section of the RM. b) Diffraction output viewed from the waveguide.

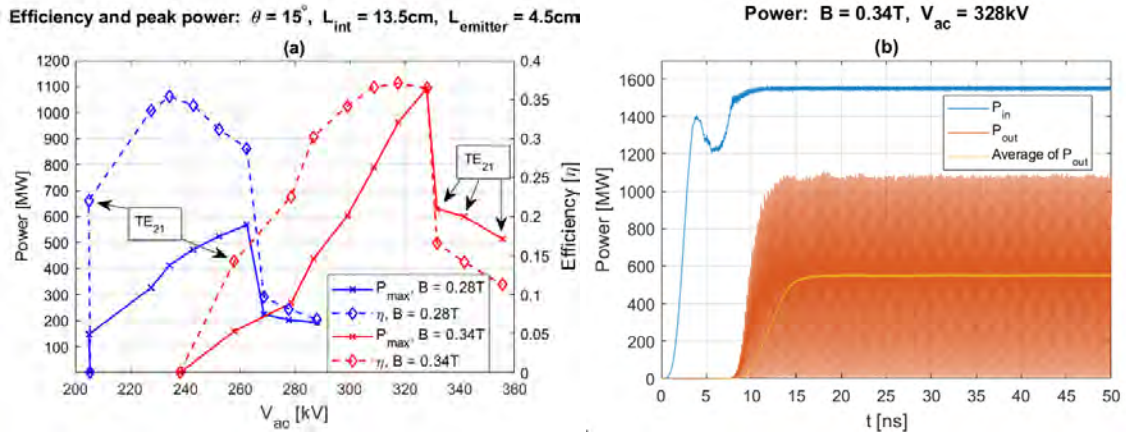


Figure 2. a) Double y-axis graph showing peak output power (left y-axis) and efficiency (right y-axis) for $B = 0.28 T$ and $B = 0.34 T$. b) Input, output, and average output power for the highest performing case.

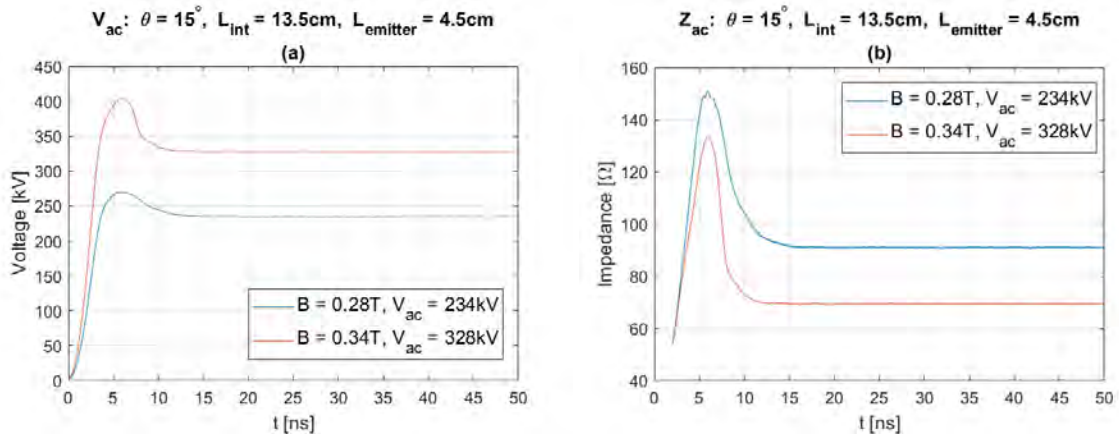


Figure 3. Voltage (a) and impedance (b) over the A-K gap for the best cases for $B = 0.28 T$ and $B = 0.34 T$.

References

- [1] M. I. Fuks and E. Schamiloglu, "70% efficient relativistic magnetron with axial extraction of radiation through a horn antenna," *IEEE Transactions on Plasma Science*, vol. 38, no. 6, pp. 1302–1312, 2010.
- [2] C. Leach, S. Prasad, M. I. Fuks, J. Buchenauer, J. W. McConaha, and E. Schamiloglu, "Experimental demonstration of a high-efficiency relativistic magnetron with diffraction output with spherical cathode endcap," *IEEE Transactions on Plasma Science*, vol. 45, no. 2, pp. 282–288, 2017.
- [3] W. Thunberg, "Particle simulation and optimization of a relativistic magnetron for HPM applications, M.Sc thesis, Uppsala University, Uppsala," 2022.